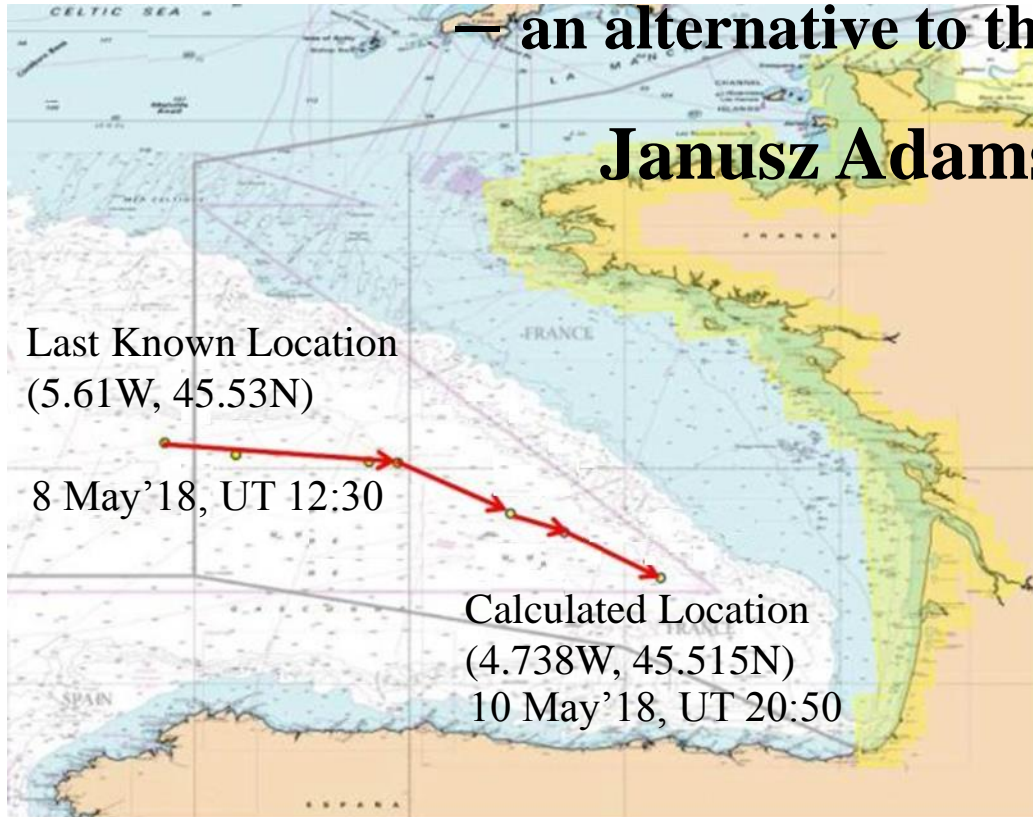


# The use of Pulsars for Ship Navigation

— an alternative to the sextant

**Janusz Adamson**

Scenario



- Severe storm in Bay of Biscay
- Rescue operations suspended
- Total power failure
- Natural, human interference
  - Communications loss
  - No GNSS/GPS signal
  - No radar
- Cloudy, sextant useless

Battery power available - for essential functions

Ship's position estimated using Dead Reckoning

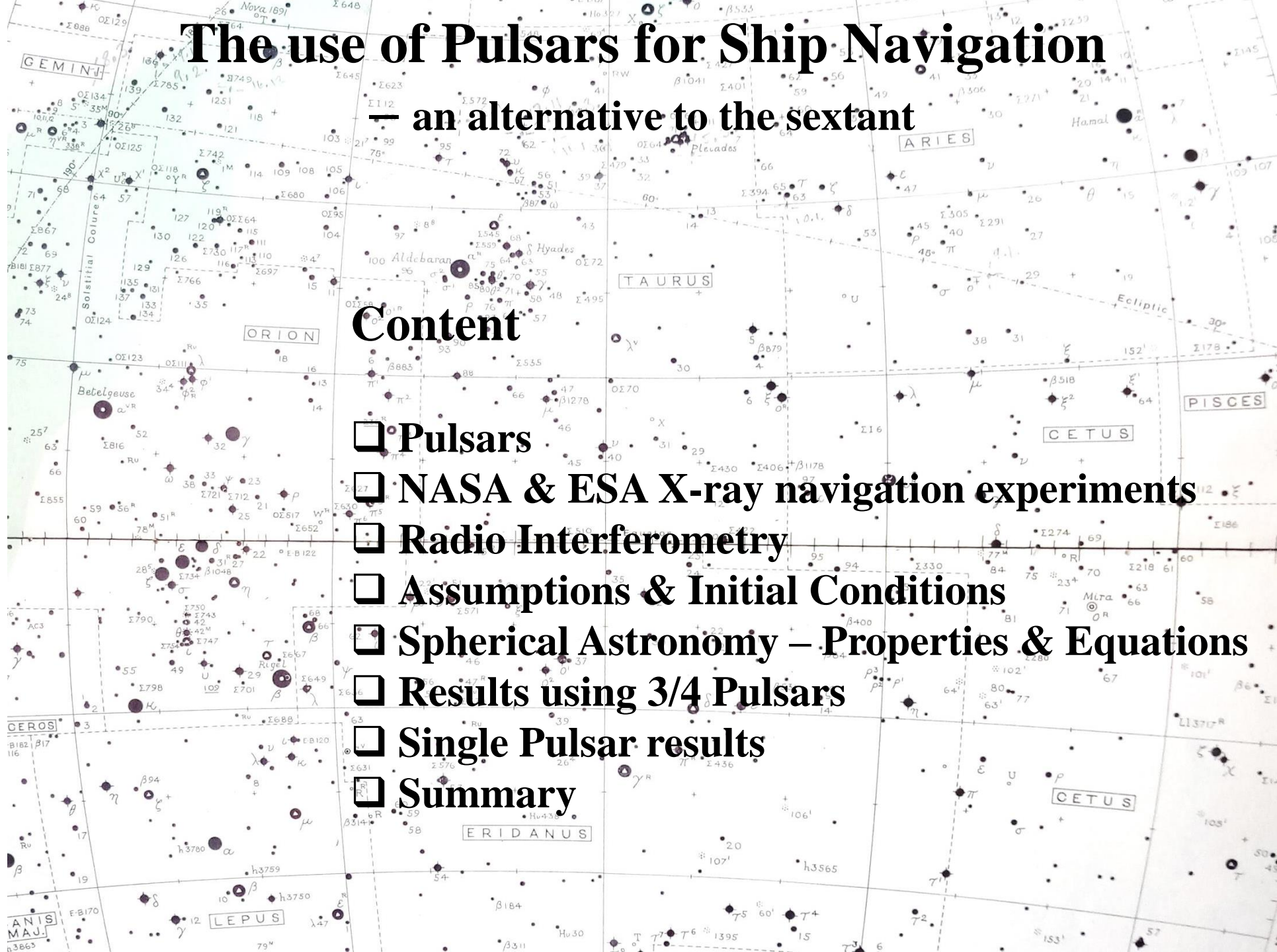


# The use of Pulsars for Ship Navigation

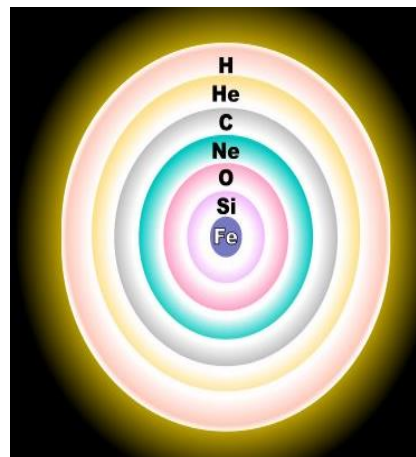
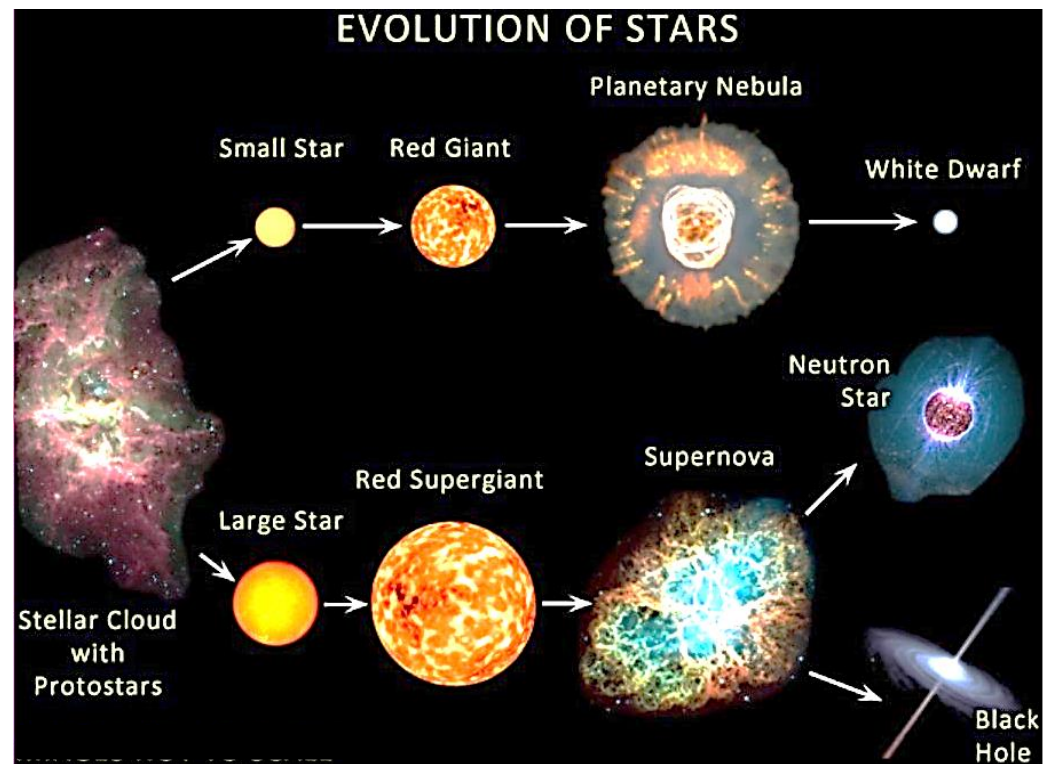
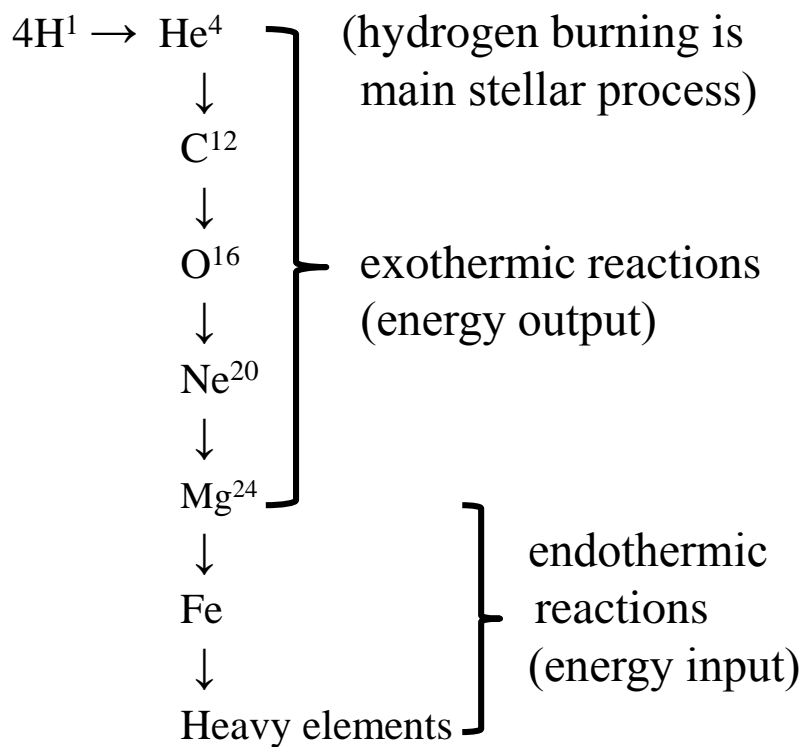
— an alternative to the sextant

## Content

- ❑ Pulsars
- ❑ NASA & ESA X-ray navigation experiments
- ❑ Radio Interferometry
- ❑ Assumptions & Initial Conditions
- ❑ Spherical Astronomy – Properties & Equations
- ❑ Results using 3/4 Pulsars
- ❑ Single Pulsar results
- ❑ Summary

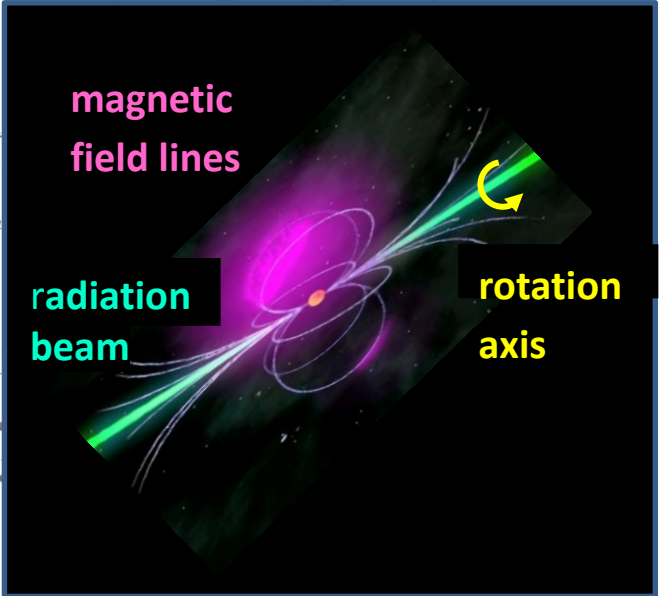
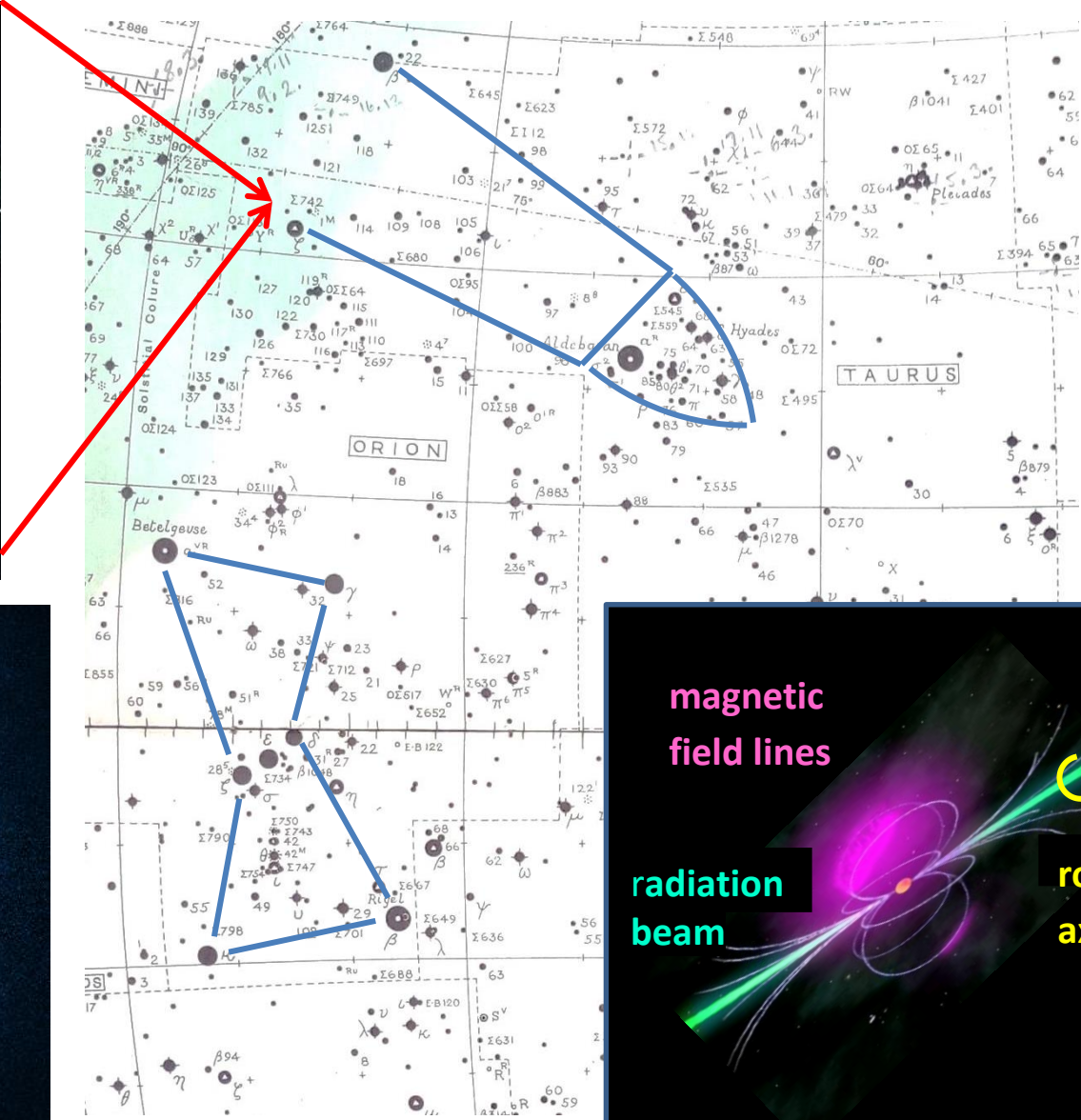
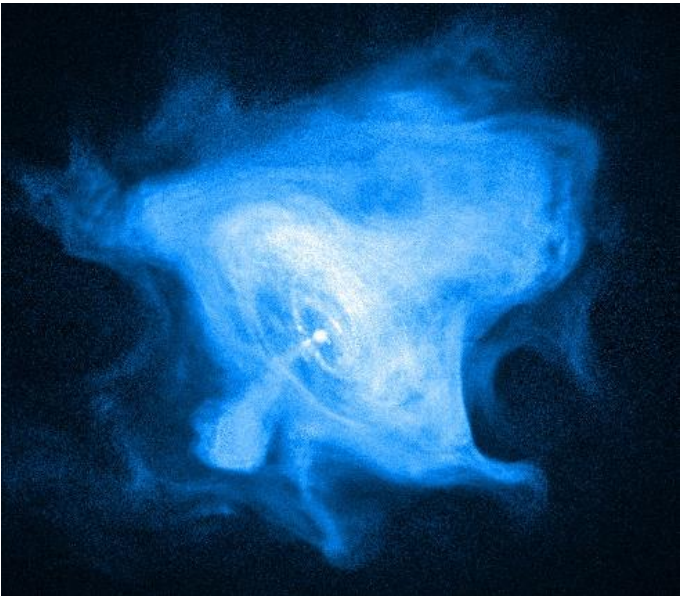
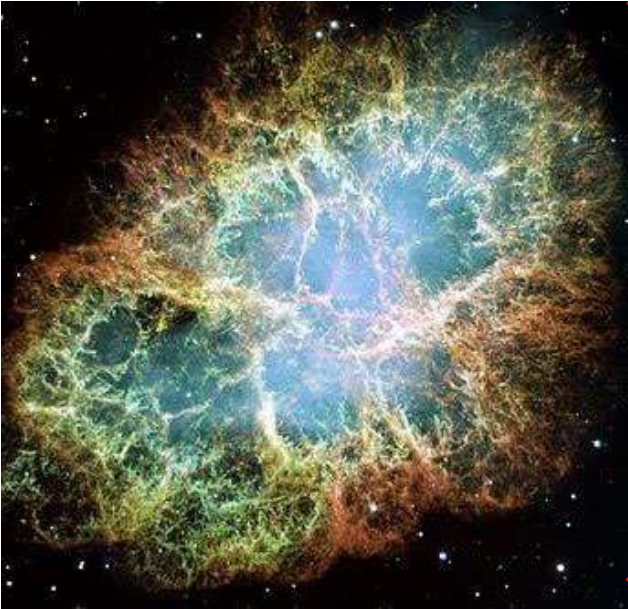


# Stellar Nuclear Reactions – basic process



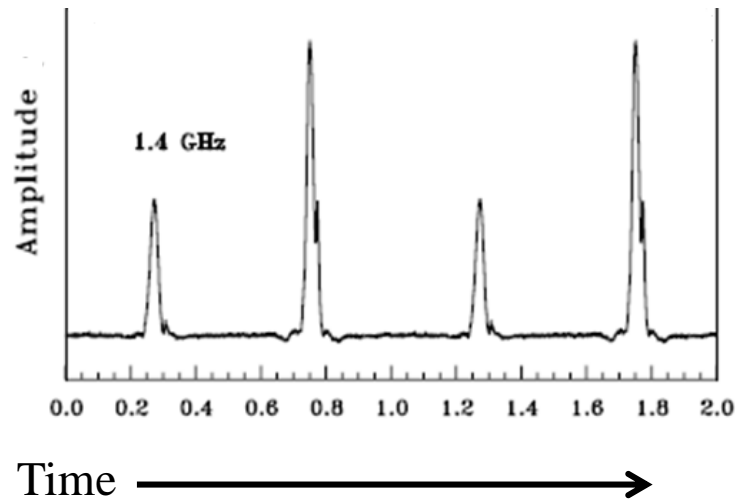
Star Type	Mass
White Dwarf	< 1.4 Solar Mass
Neutron Star	> 1.4 Solar Mass < 3.8
Black Hole	> 3.8 Solar Mass

# Crab Nebula Pulsar – Best known Pulsar (rotating neutron star)

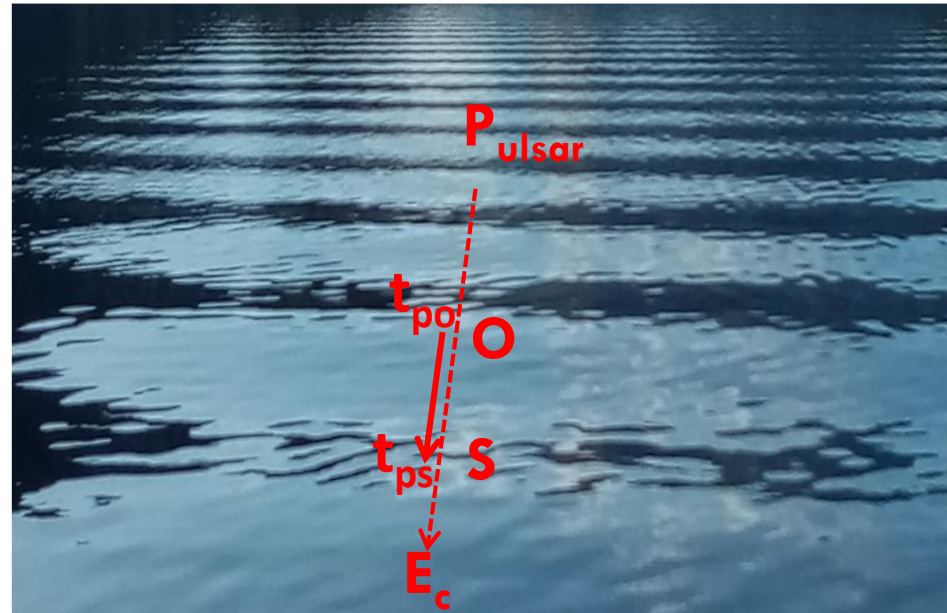


# Use of Pulsars for ship navigation

Arrival time of pulses can be predicted to a very high precision because of their long term timing stability ( $\sim 1$  in  $10^{13}$ )



Periodic pulses over many Pulsar rotation cycles

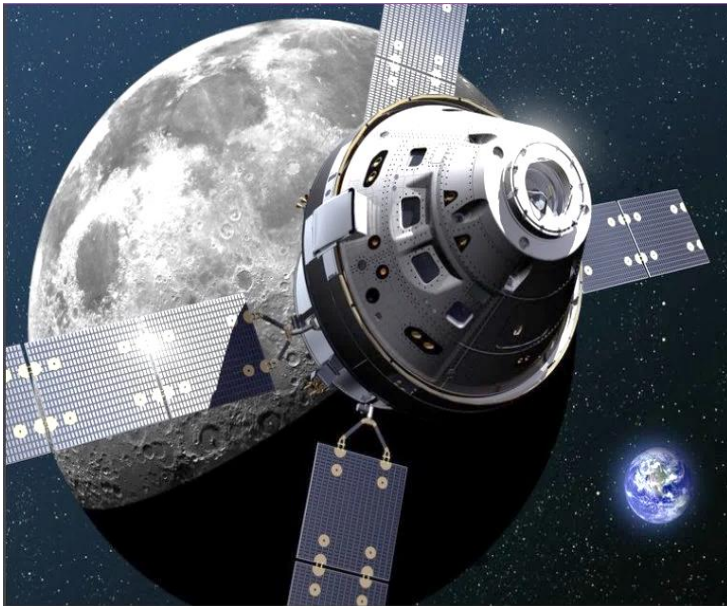


$$\text{distance} = (t_{ps} - t_{po}) \times c$$

# NASA X-ray Navigation Experiment



NICER (Neutron Star Interior Composition Explorer)/ SEXTANT (Station Explorer for X-ray Timing and Navigation Technology) experiment on the International Space Station (ISS)



Orion manned spacecraft

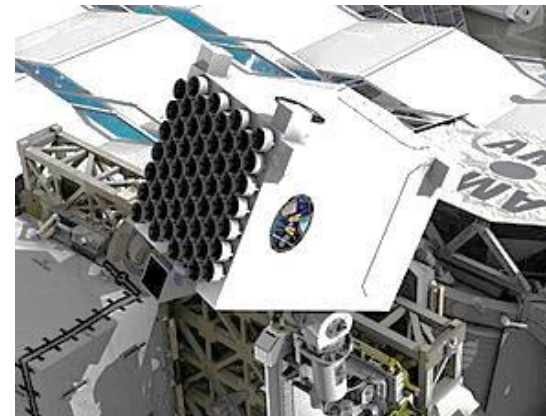
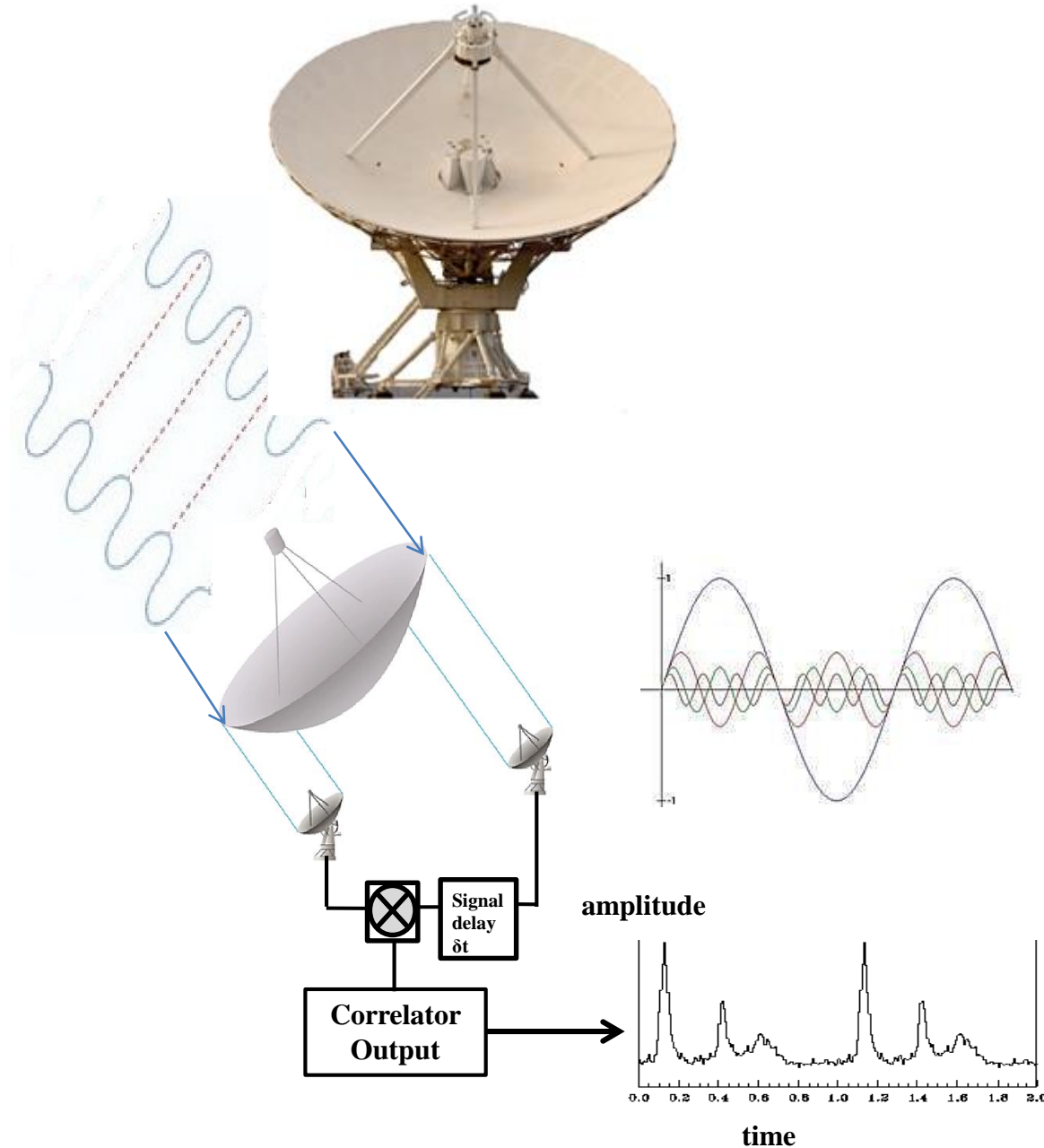


Illustration of NICER phased-array antenna aboard the ISS

# Radio telescopes – radio interferometry



Parkes 65m antenna too large, heavy, cumbersome

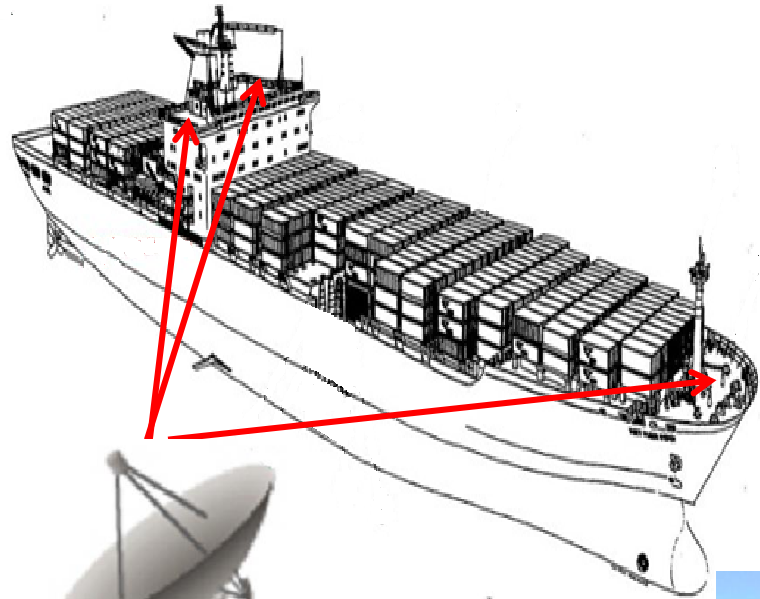
Radio interferometric approach

Virtual antenna with area equal to size of cluster

Signals are amplified, digitized at the antennas and then integrated from a cluster of radio telescopes in the correlator.

Signal integration required before Pulsar pulse timing difference measurements can begin

# Pulsar-Based Ship Navigation – potential superstructure locations for 3 or 9 x 10m<sup>2</sup> radio antennas??



Signal integration time for Parkes radio telescope 60s - 120s. Timing measurement accuracy 1 in 10<sup>13</sup>s

(Antenna area)<sup>2</sup>  $\propto$  (integration time)<sup>-1</sup>

10<sup>2</sup>m radio antenna signal integration time  $\geq 2$ min. Timing measurement accuracy 1 in 10<sup>6</sup>s required

Antenna tracking based on Type 45 Destroyer naval gun motion and positioning system in all sea conditions

# Assumptions & Initial Conditions

- Pulse timing measurement accuracy of  $10^{-6}$  s (to match NASA X-ray experiments) equates to a distance error of  $\pm 1$ km
- Earth is a geoid/ellipsoid, but assumed a spheroid at specified locations (e.g. ship's location) during pulse timing measurements; angular error  $\approx 1.2''$  arc
- Geocentric radius rounded to 1km
- Ship stationary during pulse timing measurements, drift error  $\approx 240$ m
- Unknown  $r_s$  value assumed as last known ship's value, error  $< 1$ m
- GMST  $\approx$  GAST = GST position error  $\approx 30$ m
- Greenwich chosen as reference location instead of Jodrell Bank
- Pulsar radio signal delays (due to Earth's atmosphere) are ignored

$\phi$  N

45.59° —

45.58° —

45.57° —

45.56° —

45.55° —

45.54° —

45.53° —

45.52° —

45.51° —

45.50° —

last known position on  
08/05/2018 at UT 12:30  
 $\theta = 5.61^\circ\text{W}$ ,  $\phi = 45.53^\circ\text{N}$

calculated location on  
10/05/2018 at UT 20:50  
( $4.738^\circ\text{W}$ ,  $45.515^\circ\text{N}$ )

1' of arc = 1 nautical miles  
0.1° of arc = 6 nautical miles

5.60°

5.50°

5.40°

5.30°

5.20°

5.10°

5.00°

4.90°

4.80°

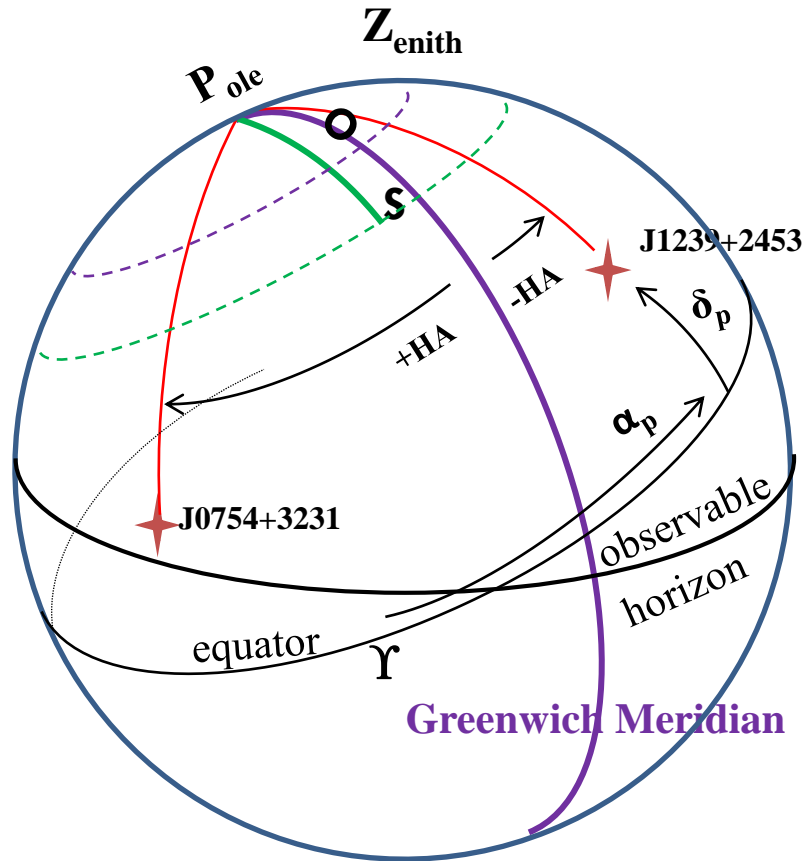
4.70°

4.60°

4.50°

$\theta$  W

# Spherical Astronomy – basic parameters



$(\theta_s, \varphi_s)$  = Ship's longitude & latitude

$HA_p$  = Hour Angle of Pulsar

G.S.T. = Greenwich Sidereal Time

G.S.T. =  $HA_p + RA_p$

$\alpha_p$  = Pulsar's Right Ascension ( $RA_p$ )

$\delta_p$  = Pulsar's Declination

$\Upsilon$  = First Point of Aries (equinox)

G.S.T. = GMST + equ. of equinoxes = GAST

$r$  = geocentric radius

$\varepsilon$  =  $1/298.257$

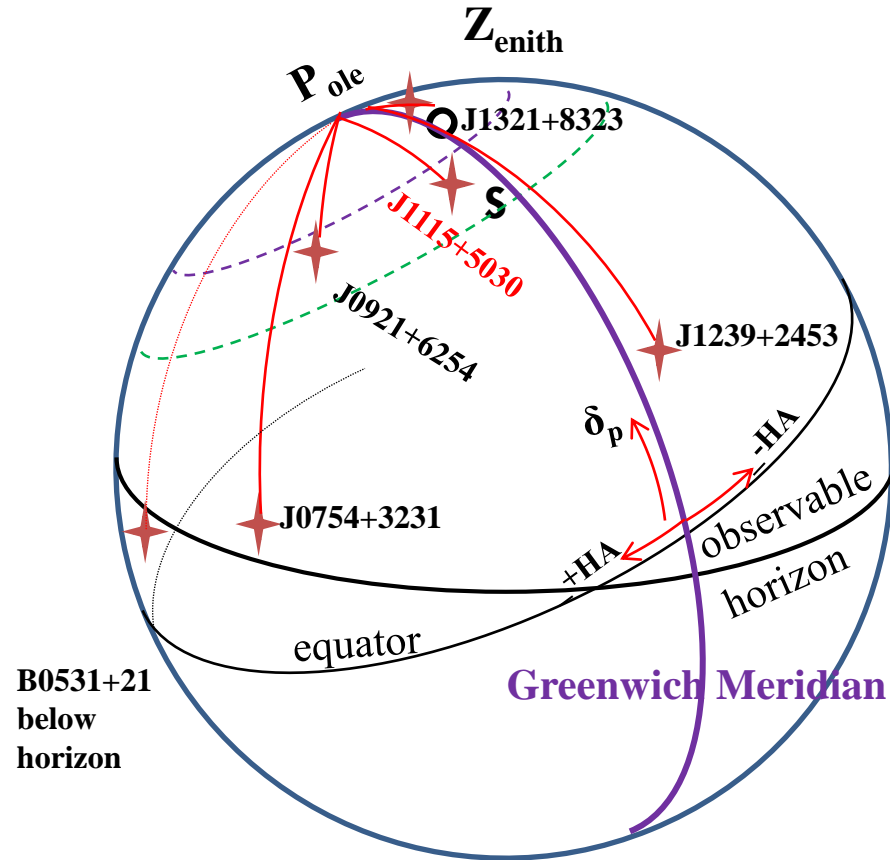
## Sign convention

Longitude east, Greenwich least (i.e. -ve)

Longitude west, Greenwich best (i.e. +ve)

# Pulsar locations

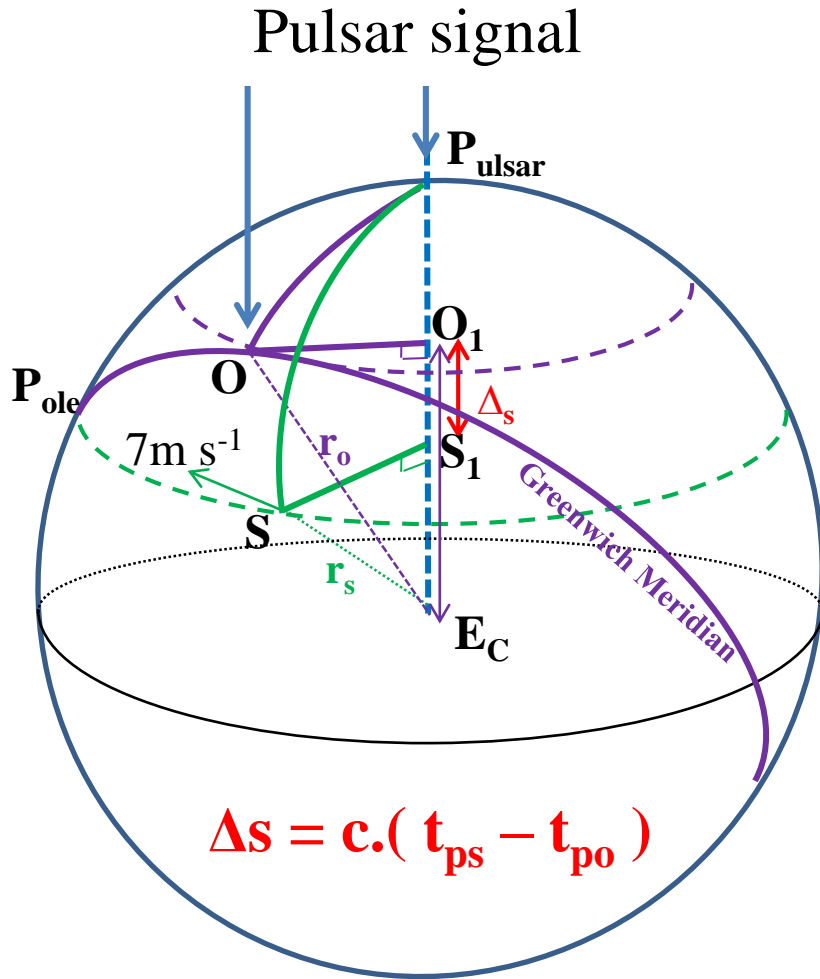
– selected for illustration purposes only



Date & Time	10 <sup>th</sup> May 2018	UT 20:50
Pulsar ID	Hour Angle (HA)	Dec ( $\delta_p$ )
J2000 notation	From GM	(degrees)
J0754+3231	62.43396°	32.53228°
<b>J1115+5030</b>	12.19350°	<b>50.50341°</b>
J0921+6254	40.79460°	62.90387°
J1239+2453	-8.81509°	24.89702°
J1321+8323	-19.33892°	83.39414°
<b>Crab Nebula Pulsar</b>		
<b>B0531+21</b>	97.47029°	22.01447°

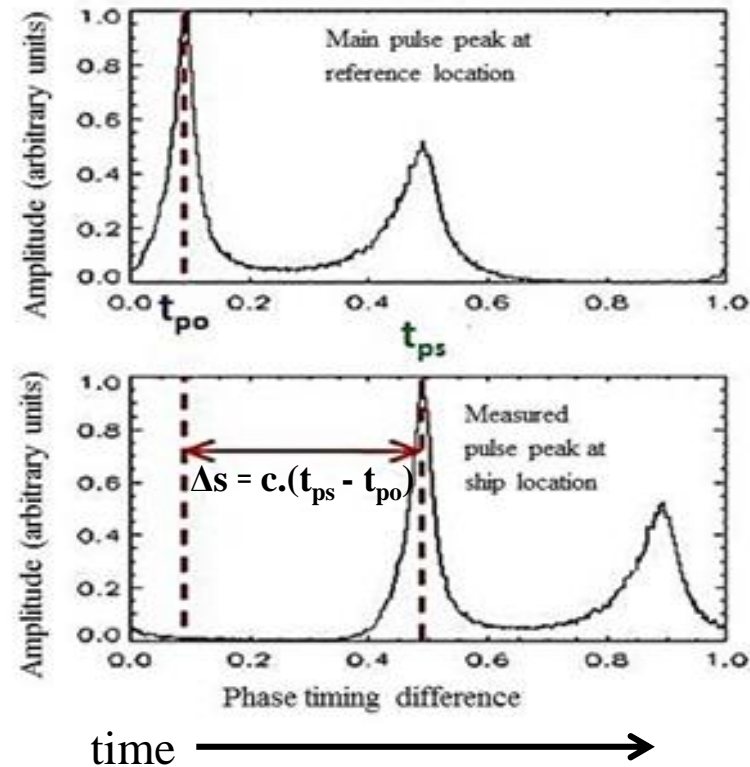
3 Pulsars = unique solution  
 4+ Pulsars = over-determined solution

# Pulsar – Pulse Peak Timing Difference Measurements



$O_1$  &  $S_1$  are projections of reference observatory (O) and unknown ship position (S) onto the Pulsar-Earth centre line

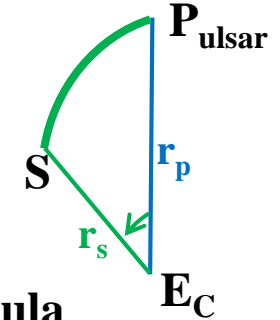
Date	10 <sup>th</sup> May 2018	UT 20:50
J2000notation	Timing difference	Distance $\Delta s$
J0754+3231	$\approx 7.61 \times 10^{-4}$ s	$-228 \pm 1$ km
J1115+5030	$\approx 4.0 \times 10^{-5}$ s	<b><math>-12 \pm 1</math> km</b>
J0921+6254	$\approx 3.77 \times 10^{-4}$ s	$113 \pm 1$ km
J1239+2453	$\approx 6.57 \times 10^{-4}$ s	$-197 \pm 1$ km
J1321+8323	$\approx 1.321 \times 10^{-3}$ s	$396 \pm 1$ km



# Spherical Astronomy – properties & equations

1' of arc = 1 nautical mile  
 0.1° of arc = 6 nautical miles

great circle arc( $SP_{\text{ulsar}}$ ) = angle( $SE_C P_{\text{ulsar}}$ )



**spherical trigonometric cosine formula**

$$\cos(\text{arc}SP_{\text{ulsar}}) = \cos(90 - \varphi_s)\cos(90 - \delta_p) - \sin(90 - \varphi_s)\sin(90 - \delta_p)\cos(-HA_p + \theta_s)$$

**basic trigonometric function**

$$d_o = r_o \cos(OE_C P_{\text{ulsar}})$$

$$d_s = r_s \cos(SE_C P_{\text{ulsar}})$$

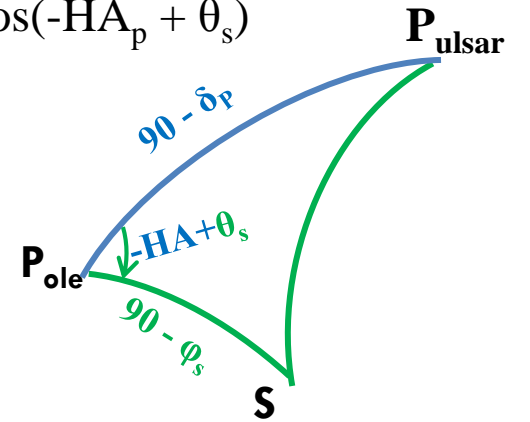
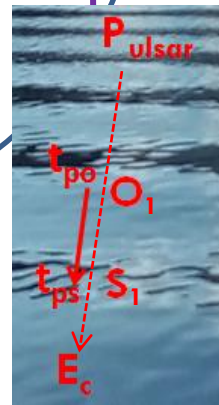
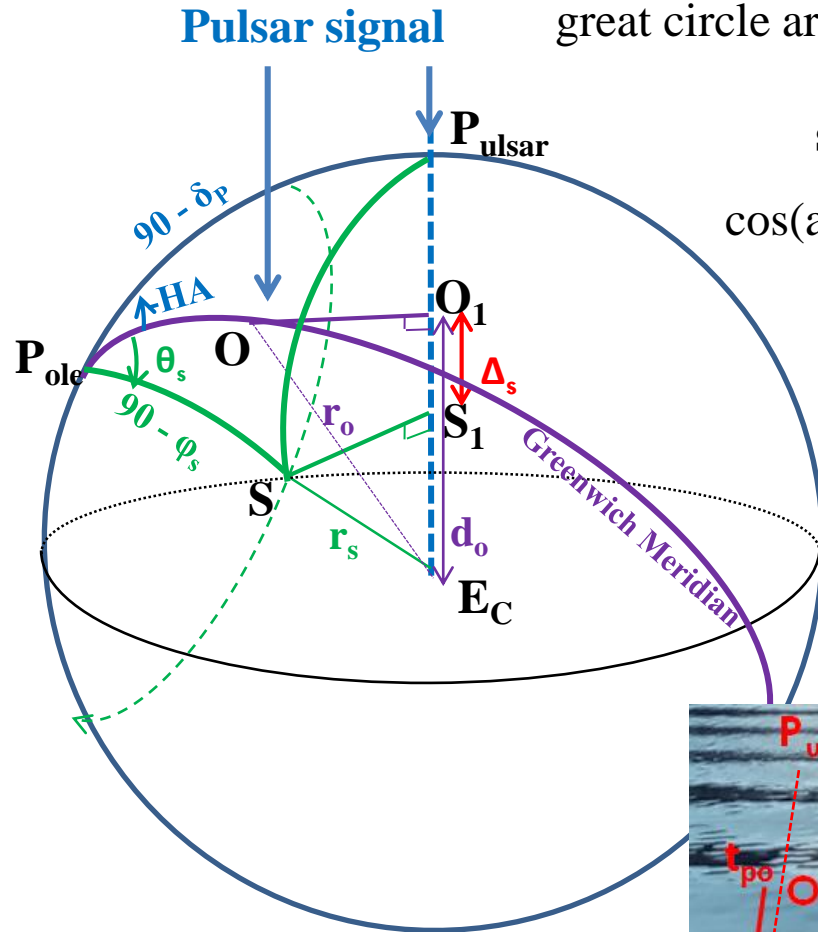
$$r \approx 6378(1 - \epsilon \sin^2 \varphi) \text{ km}$$

$$d_o = \overrightarrow{E_C O_1}$$

$$d_s = \overrightarrow{E_C S_1}$$

$$d_s = d_o - \Delta s$$

$$\Delta s = (t_{ps} - t_{po}) \times c$$



**Sign convention**

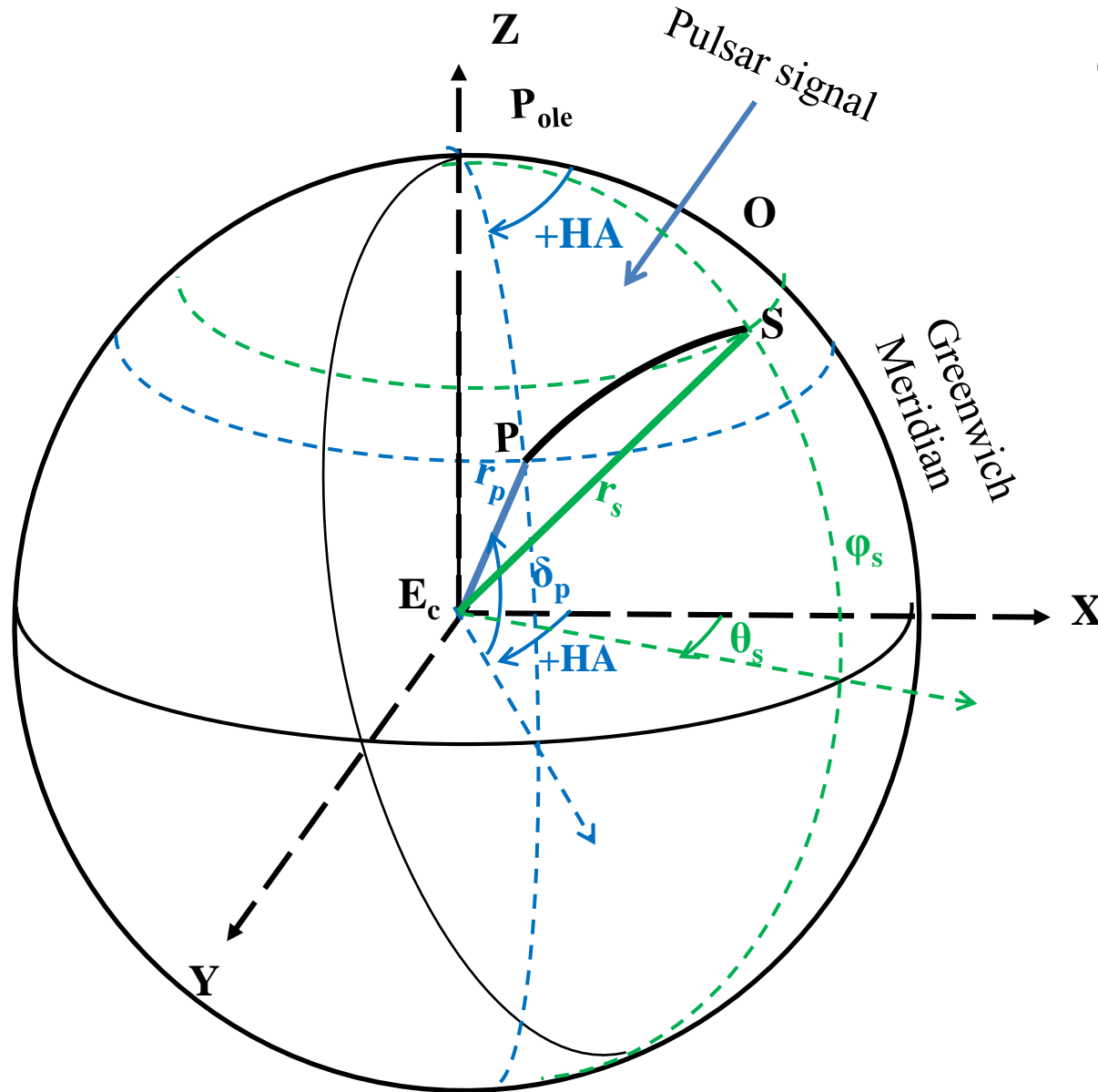
Longitude east -ve

Longitude west +ve

H.A. east -ve

H.A. west +ve

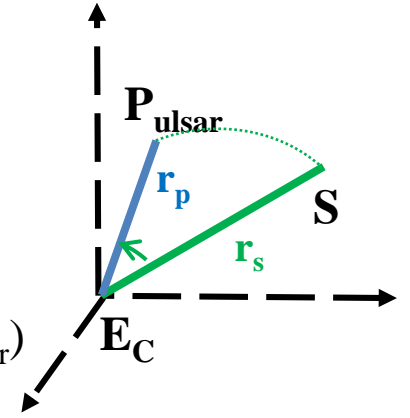
# Vector scalar product



$$\cos(\text{SE}_C\text{P}_{\text{ulsar}}) = \frac{\mathbf{r}_s \cdot \mathbf{r}_p}{|\mathbf{r}_s| |\mathbf{r}_p|}$$

and  $d_s = r_s \cos(\text{SE}_C\text{P}_{\text{ulsar}})$

so  $|\mathbf{r}_p| d_s = \mathbf{r}_s \cdot \mathbf{r}_p$   
 $= x_s \cdot x_p + y_s \cdot y_p + z_s \cdot z_p$



coordinate transformation

$$\begin{aligned} x_s &= r_s \cos(\varphi_s) \cos(\theta_s) \\ y_s &= r_s \cos(\varphi_s) \sin(\theta_s) \\ z_s &= r_s \sin(\varphi_s) \end{aligned}$$

$$\begin{aligned} x_p &= r_p \cos(\delta_p) \cos(\text{HA}_p) \\ y_p &= r_p \cos(\delta_p) \sin(\text{HA}_p) \\ z_p &= r_p \sin(\delta_p) \end{aligned}$$

# Solution – 4 signal timing measurements

Solutions in matrix form are written as

$$\begin{bmatrix} A_1 & B_1 & C_1 \\ A_2 & B_2 & C_2 \\ A_3 & B_3 & C_3 \\ A_4 & B_4 & C_4 \end{bmatrix} \begin{bmatrix} x \\ yf \\ yg \end{bmatrix} = \begin{bmatrix} D_1 \\ D_2 \\ D_3 \\ D_4 \end{bmatrix}$$

where

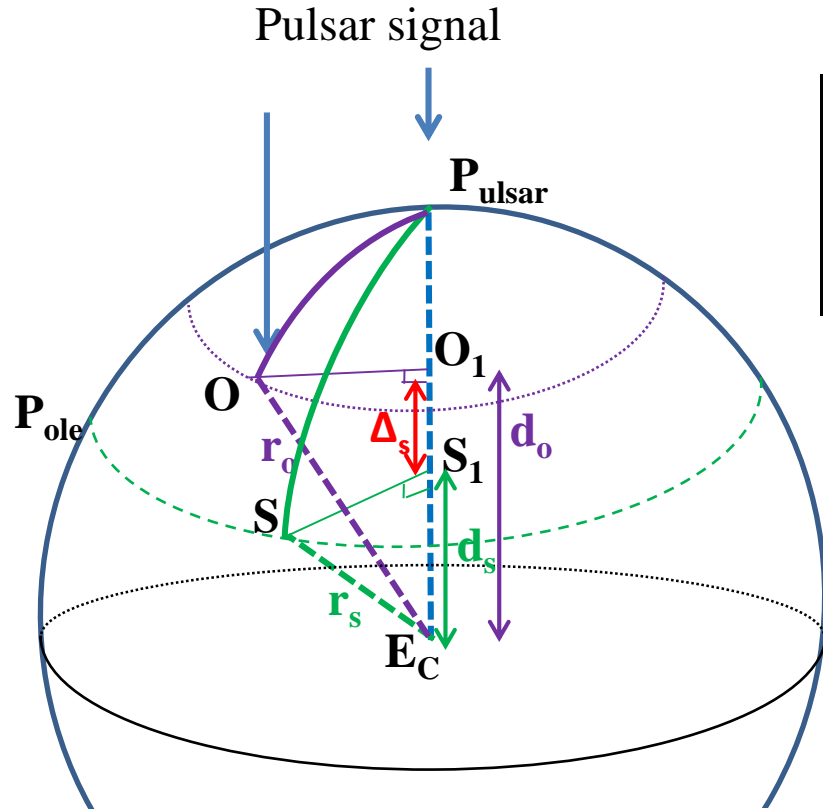
A, B, C, D are calculated values

x, y, f, g are unknown functions for  $(\theta_s, \varphi_s)$

change in  $r_s$  is minimal, hence ignored

A solution for x, y, f, g, can be written as

$$\begin{array}{c} \overline{x} \\ \left| \begin{array}{ccc} D_1 & B_1 & C_1 \\ D_2 & B_2 & C_2 \\ D_3 & B_3 & C_3 \end{array} \right| \end{array} = \begin{array}{c} \overline{yf} \\ \left| \begin{array}{ccc} A_1 & D_1 & C_1 \\ A_2 & D_2 & C_2 \\ A_3 & D_3 & C_3 \end{array} \right| \end{array} = \begin{array}{c} \overline{yg} \\ \left| \begin{array}{ccc} A_1 & B_1 & D_1 \\ A_2 & B_2 & D_2 \\ A_3 & B_3 & D_3 \end{array} \right| \end{array} = \begin{array}{c} \overline{1} \\ \left| \begin{array}{ccc} A_1 & B_1 & C_1 \\ A_2 & B_2 & C_2 \\ A_3 & B_3 & C_3 \end{array} \right| \end{array}$$



# Ship's position on 10/05/2018 at UT 20:50

1' of arc = 1 nautical mile  
0.1° of arc = 6 nautical miles

4 significant figure  
computations

7 significant figure  
computations

$\phi$  N

45.59° —  
45.58° —  
45.57° —  
45.56° —  
45.55° —  
45.54° —  
45.53° —  
45.52° —  
45.51° —  
45.50° —

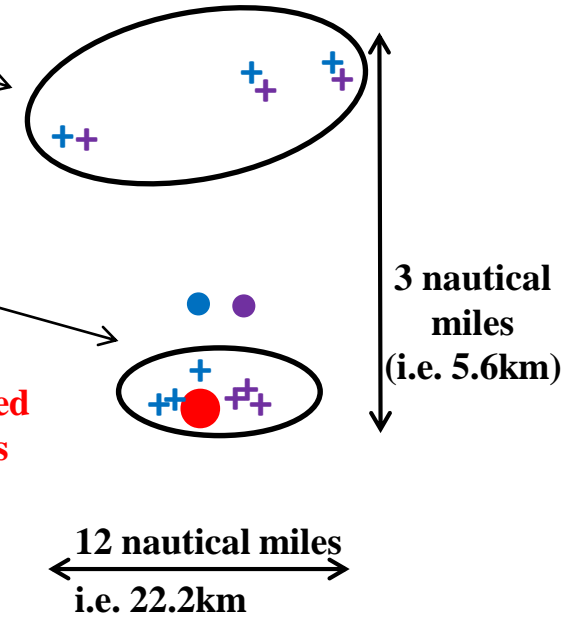
last known position on  
08/05/2018 at UT 12:30  
 $\theta = 5.61^\circ$ ,  $\phi = 45.53^\circ$



computations based on  
 $10^{-5}$  sec measurement  
accuracy

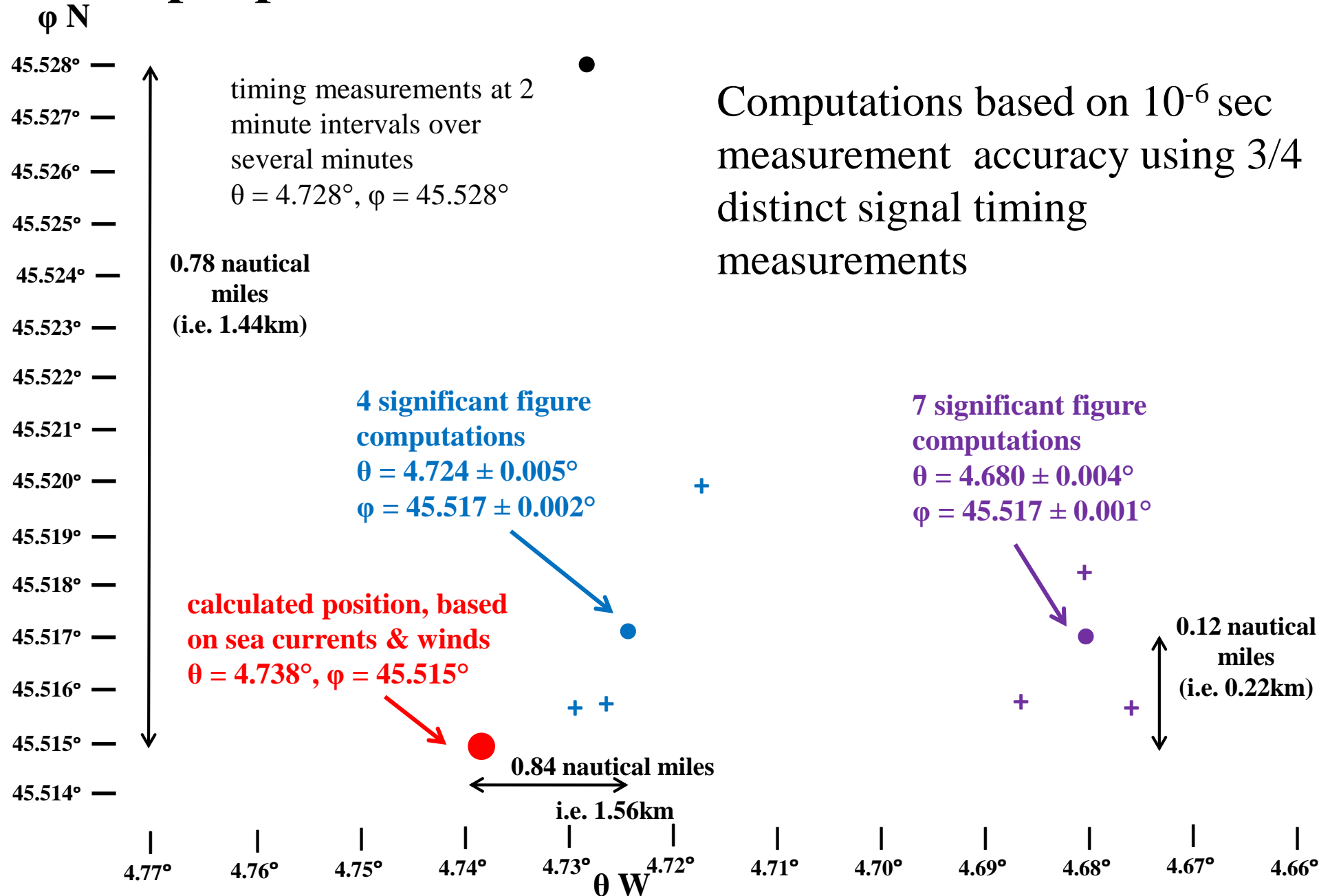
computations based  
on  $10^{-6}$  sec  
measurement  
accuracy

calculated position, based  
on sea currents & winds  
 $\theta = 4.738^\circ$ ,  $\phi = 45.515^\circ$



5.60° 5.50° 5.40° 5.30° 5.20° 5.10° 5.00° 4.90° 4.80° 4.70° 4.60° 4.50°  
 $\theta$  W

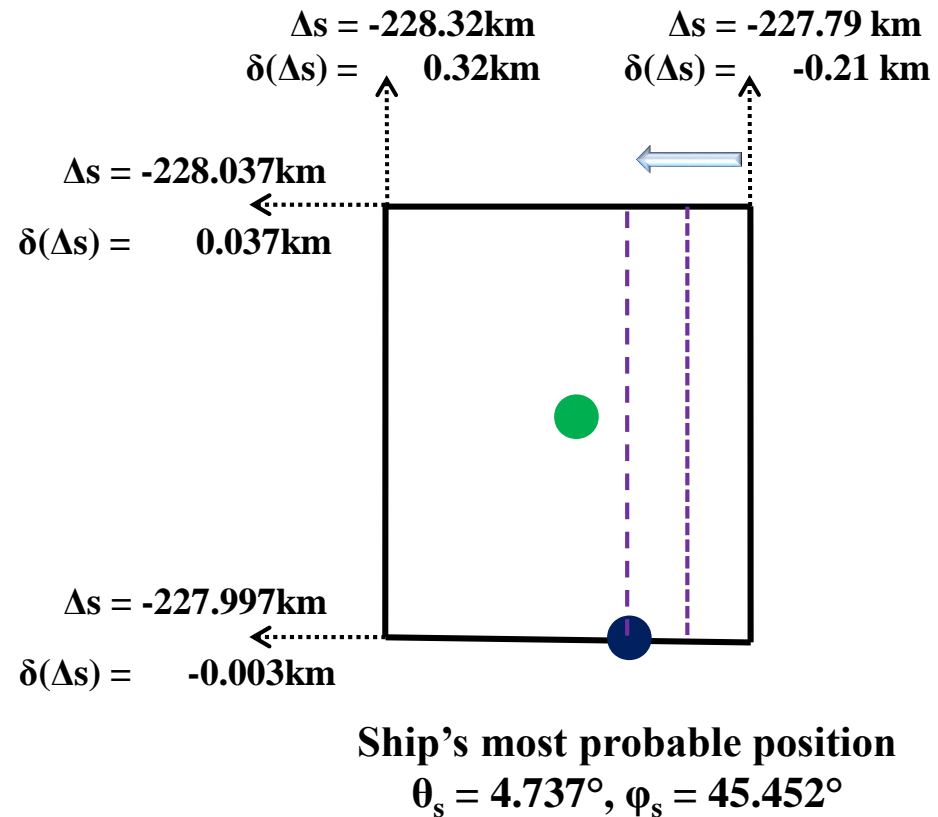
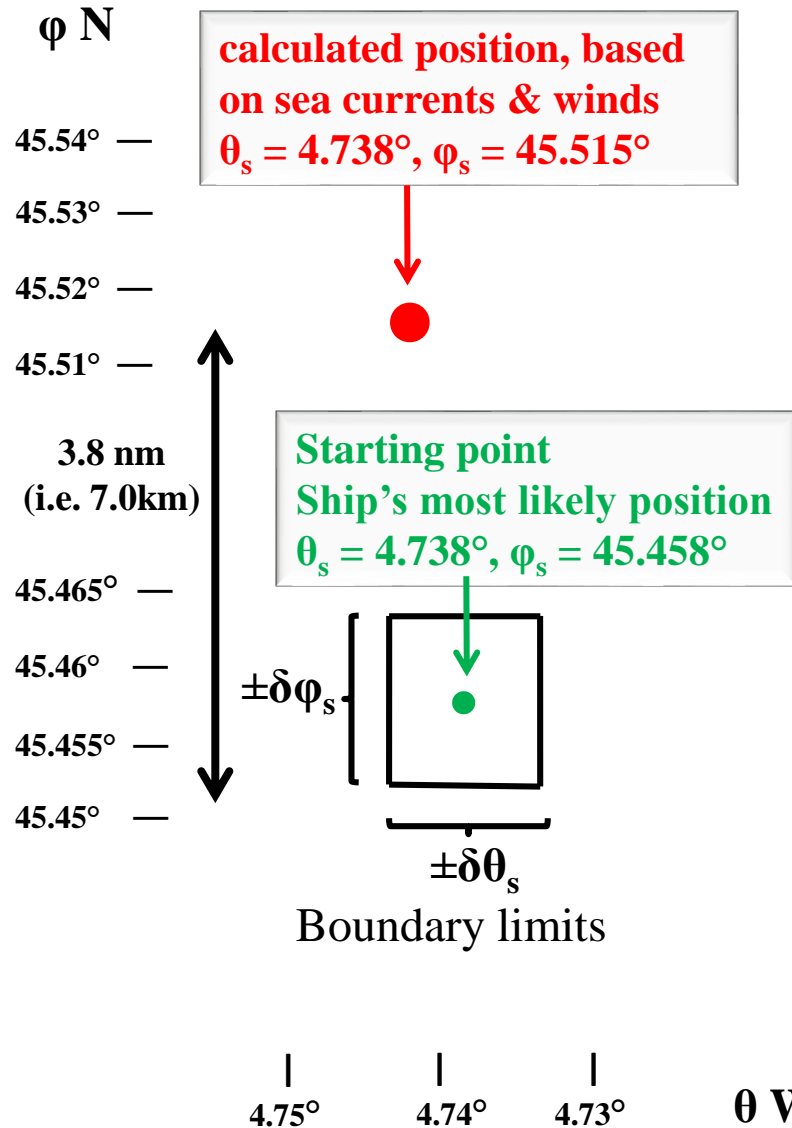
# Ship's position on 10/05/2018 at UT 20:50





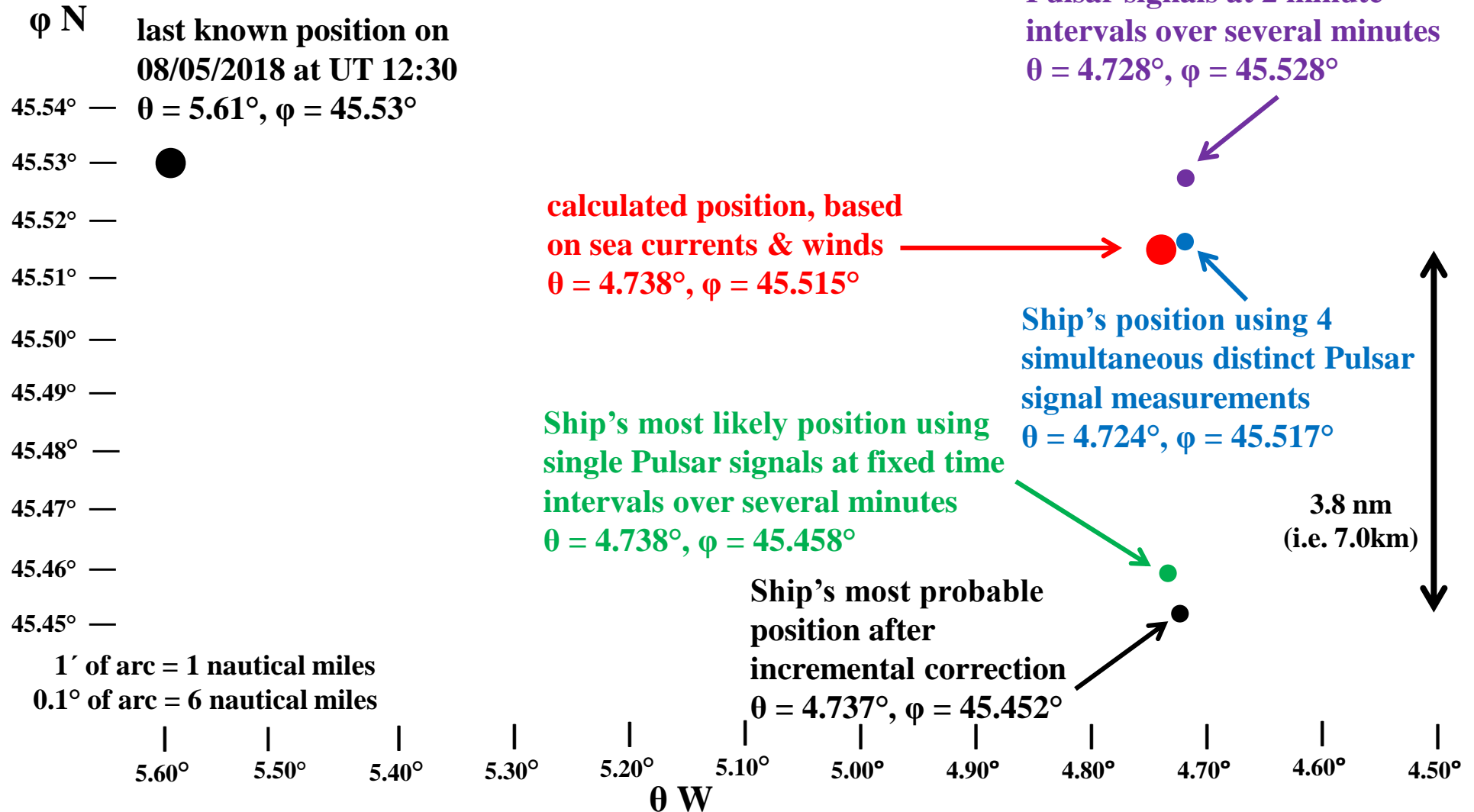
# Incremental Change – using Pulsar J0754+3231

**Method** use Taylor's Theorem to calculate  $\delta\theta$ ,  $\delta\phi$  followed by Divide & Conquer



# Ship's position on 10/05/2018 at UT 20:50

Computations based on  $10^{-6}$  sec measurement accuracy



# The use of Pulsars for Ship Navigation

– an alternative to the sextant

## Summary

- ❑ Earth's atmosphere opaque to X-rays.
- ❑ An interferometric approach using a cluster of small radio antennas, to be located on the ship's superstructure.
- ❑ Position accuracy achieved to within 2km.
- ❑ Single Pulsar signal calculations provide a ship's position to within 7km.
- ❑  $10^{-6}$  pulse profile resolutions to be comparable with NASA's and ESA's spacecraft navigation experiments.
- ❑ Order of magnitude position improvement could be achieved using  $10^{-7}$  pulse profile measurement resolution.
- ❑ Challenge – provide improved position accuracies in the next few years.